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(54) Title: METHOD AND APPARATUS FOR MULTIUSER-INTERFERENCE REDUCTION
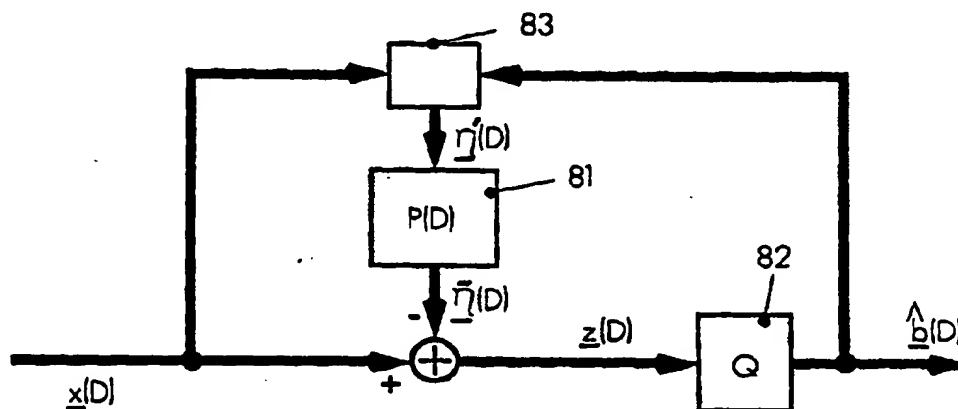
(57) Abstract

The present invention concerns an apparatus and method for reducing the multiuser-interference of input signals. The apparatus in accordance with the present invention comprises a multivariate predictor (81) and a decision quantizer (82), said multivariate predictor (81) operating on interference signals $\underline{\eta}'(D)$ provided by means for extracting interference signals (83), said interference signals $\underline{\eta}'(D)$ being obtained from said input signals and output signals $\underline{\hat{b}}(D)$ which are available at an output of said decision quantizer (82) and fed back from there to said means for extracting interference signals (83).

DESCRIPTION

Method and Apparatus for Multiuser-Interference Reduction

TECHNICAL FIELD

The present invention relates to a method and apparatus for reducing the multiuser-interference in Code Division Multiple Access (CDMA) multi-channel communication systems, and in particular, in CDMA cellular radio communication systems. The present invention is also applicable in CDMA Infra Red (IR) networks.

BACKGROUND OF THE INVENTION

Wireless communication systems, in particular cellular radio telephone communication systems and diffused Infra Red (IR) systems, become more and more important because they increase mobility and offer wireless connectivity to telephone and computer users almost everywhere. While the latter ones are usually deployed indoors, e.g. for the interconnection of computers and servers, the cellular radio communication systems, e.g. the analog AMP systems in the US and the digital GSM system in Europe, facilitate mobile communication and data exchange in almost all metropolitan areas. It is expected that the emerging Personal Communications Networks (PCN) will encompass a wider range of communications capabilities than those represented by current analog or digital cellular mobile radio technology. High traffic capacity and low power consumption are two important issues in the emerging new cellular systems.

Currently, channel access in cellular radio telephone communication systems is achieved by using Frequency Division Multiple Access (FDMA) and Time Division Multiple Access (TDMA) methods. In FDMA-based

1 systems, the capacity is limited by the number of available frequency subbands, whereas the capacity of TDMA systems is limited by the number of slots per frame carrying the transmitted signals.

5 In contrast, Code Division Multiple Access (CDMA) allows signals to overlap in both frequency and time. Thus, all CDMA signals share the same frequency spectrum. In either time or frequency domain, the multiple access signals appear to be on top of each other. A CDMA-based communications system model is illustrated in Figure 4. The data stream of the kth user

10 $\{b_k(n)\}$, e.g. speech or data, to be transmitted is modulated by a user specific signal $s_k(t)$. Each signal $s_k(t)$ corresponds to a unique spreading code $\underline{c}_k$. A plurality of spread spectrum signals is modulated and transmitted on a radio frequency (RF) carrier wave. At the receiver, the composite signal $r(t)$ is demodulated and correlated with a selected

15 spreading code $\underline{c}_k$. The correlation by the user specific spreading code isolates and decodes the corresponding data signal.

There are a number of advantages associated with the CDMA technology. The capacity of CDMA-based systems is projected to be several times

20 higher than that of existing analog FDMA systems. In addition, CDMA is resistant to multi-path interference and fading. Furthermore, the scrambled format of CDMA signals makes it difficult and costly to eavesdrop or track calls, insuring greater privacy for users and providing greater immunity from air time fraud.

25

Conventional CDMA systems are multiuser-interference limited, whereas the above described TDMA and FDMA systems are primarily bandwidth limited. Thus, in practical implementations of CDMA, capacity is directly related to the signal-to-interference (S/I) ratio, which is essentially a measure of the

30 multiuser interference, caused by other overlapping signals. The problem to be solved, therefore, is how to further increase system capacity and still be able to maintain a reasonable S/I ratio so that signal decoding can be carried out efficiently and accurately.

1

Conventional code-division multiple-access cellular and microcellular wireless systems use long spreading codes, i.e. sequences whose period is much longer than the data symbol duration, employ complex powerful

5   convolutional codes to mitigate the effect of multiuser interference, and rely on power control strategies to remedy the "near-far problem". However, as the number of simultaneous transmissions in a system of fixed bandwidth increases, or as the relative power levels of the different user signals become disparate (near-far problems), a high performance penalty is

10 observed. The sensitivity of these systems to the multiuser interference and to the "near-far problem" can substantially reduce the capacity of the overall system. The "near-far problem" is more critical on the asynchronous uplink, i.e. the communication from a mobile station (MS) to a base station (BS), where the different user signals could arrive with different power levels. In

15 contrast, on the synchronous downlink, from a BS to a MS, the multiuser interference is primarily due to simultaneous transmissions by neighboring base stations.

Some conventional CDMA systems, in particular the receivers therein that

20 are relevant in the present context, are described below. The performance limitations of a conventional asynchronous CDMA system have been discussed by M. B. Pursley in the article "Performance Evaluation for Phase-Coded Spread Spectrum Multiple-Access Communication- Part I: System analysis", IEEE Transactions on Communications, Vol. COM-25, pp.

25 795-799, Aug. 1977.

The optimum multiuser receiver consisting of a bank of matched filters followed by a Viterbi detector which performs joint maximum likelihood sequence estimation (MLSE) has been considered in "Minimum probability

30 of error for asynchronous Gaussian multiple access channels", by S. Verdú, IEEE Transactions on Information Theory, Vol. IT-32, pp. 85-96, Jan. 1986.

1   Suboptimum linear multiuser decorrelating detectors for a synchronous or asynchronous CDMA system have been presented in "Linear multiuser detectors for synchronous code-division multiple access channels", R. Lupas and S. Verdú, IEEE Transactions on Information Theory, Vol. IT-35, pp.
5   123-136, Jan. 1989. These suboptimum detectors are essentially zero-forcing (ZF) multiple-input/multiple-output linear equalizers, i.e. multiple-input/multiple-output linear filters that minimize multiuser interference using the ZF criterion. They are also known as ZF multiuser equalizers. It is shown that the decorrelating detector is near-far resistant.
10   Furthermore, it is pointed out by R. Lupas and S. Verdú in the above article that the decorrelating detector or multiuser ZF equalizer requires knowledge of the spreading codes of all users, but no explicit knowledge of the relative received signal powers.

15   A conventional multivariate decision-feedback equalizer (MDFE), which requires knowledge of the spreading codes of all users, has been disclosed in "Equalizers for multiple input/multiple output channels and PAM systems with cyclostationary input sequences", A. Duel-Hallen, IEEE Journal on Selected Areas in Communications, Vol. 10, No. 3, pp. 630-639, Apr. 1992. A
20   noise-predictive decision-feedback equalizer (NP-DFE) has been proposed in "Decision feedback equalization", C. A. Belfiore and J. H. Park, Jr., Proc. IEEE, Vol. 67, No. 8, pp. 1143-1156, Aug. 1979. However, the latter structure has been derived for only the case of a single-variable, meaning the data of only one user, corrupted by intersymbol-interference (ISI) and additive
25   noise, is detected. Such a structure is not suitable for a CDMA system.

The use of an adaptive fractional-chip spaced decision-feedback equalizer (DFE) in a CDMA system has been discussed in "Equalization for interference suppression in spread spectrum multiple access systems", M.
30   Abdulrahman, D. D. Falconer, and A. U. H. Sheikh, in Conference Records IEEE VTC 92, Vol. 1, (Denver, CO), pp. 1-4, May 1992. It was demonstrated that a single-input/single-output adaptive DFE placed in an MS receiver can mitigate the effects of multiuser interference, can perform RAKE (RAKE is a

1   code name for a receiver being described in "Digital Communications" by
J.G. Proakis, McGraw-Hill Book Company, 1983) combining of multipath
components, and also that it does not require explicit knowledge of the
interferers' spreading code. The feedback section of the DFE is using past
5   decisions from a single user and thus cannot further compensate for
multiuser-interference. In such a configuration the feedback section
eliminates only ISI (intersymbol interference).

Another CDMA system proposal is based on the technique of detection and
10   subtraction of interferers' signals in user order, also known as interference
cancellation (IC). This CDMA system proposal is disclosed in "CDMA using
interference cancellation", M. Ewerbring, G. Larsson, and P. Teder, CEC
Deliverable R2020/PKI/RI/DS/I/005/b1 (W. Granzow, ed.), pp. 141-163, 1992.
Many properties of this CDMA system proposal, however, include the fact
15   that knowledge of the users' spreading code is essential.

In US patent 5 136 612, entitled "Method and Apparatus for Reducing
Effects of Multiple Access Interference in a Radio Receiver in a Code
Division Multiple Access Communication System", another CDMA scheme is
20   disclosed. The channel capacity is increased, in accordance with this US
patent, by reduction of the effects of the multiple access interference, also
referred to as multiuser interference. The reception of CDMA radio
transmissions is in multiple stages, and the multiple access interference is
estimated after the first stage. This multiple access interference is then
25   subtracted from the original, received input, and the detection of the
intended signal is performed on the signal having the reduced multiple
access interference.

A slightly different approach is known from US patent 5 218 619, entitled
30   "CDMA Subtractive Demodulation". According to this approach, the received
information signal, i.e. the composite signal, after each information signal
has been successfully decoded, is recoded and then removed from the
composite signal. The CDMA demodulation is enhanced by decoding the

1   composite signal in the order of strongest to weakest signal strength. The
     common principle of the latter two US patents is illustrated in Figure 1,
     which shows a schematic CDMA receiver. As shown in this Figure, the
     composite signal r(t) is fed to a despreader (DS) 10, where the spreading
5   codes used at the transmitter site are employed in order to decode the
     respective information signals. These information signals are then
     forwarded to a decision quantizer (Q) 11. The detected signals are
     classified into those that are most likely correct and those that are likely not
     to be correct. The detection process is then repeated. From the decoded
10   data signal $\hat{\underline{b}}(n)$ the ones that are most likely correct are fed back to the
     spreading circuitry (S) 12 where they are recoded (spread) using the
     corresponding spreading codes. The regenerated spread waveforms are
     subtracted from the original received signal r(t) to remove part of the
     multiuser interference. Thus the outputs which initially were classified as
15   being not correct are re-detected in a second stage.

     The underlying concept of the structure described in the article of
     A. Duel-Hallen is shown in Figure 2A. It consists of a
     multiple-input/multiple-output forward filter 17 and a
20   multiple-input/multiple-output feedback filter 14. The detected data vector
     $\underline{b}(n) = (\hat{b}_1(n), ... , \hat{b}_K(n))$, representing decisions for all K users, is provided
     at the output of a decision quantizer 13 is filtered by the
     multiple-input/multiple-output feedback filter (FBF) 14. From there it is fed
     back to the quantizer's input to reduce multiuser-interference.

25
     The underlying concept of the system described by M. Abdulrahman et al. is
     shown in Figure 2B. The detected data symbols of a particular user $\hat{b}_K(n)$,
     i.e. the symbols at the output of the decision quantizer 15, are fed back via a
     single-input/single-output feedback filter 16. Note that the feedback section
30   can mitigate only ISI and not multiuser-interference.

     The "near-far" problem and the multiuser-interference are still the main
     impediments towards higher capacity

SUMMARY OF THE INVENTION

It is an object of the present invention to provide a novel structure and method for mitigating the effects of interference due to simultaneous transmissions in a CDMA system without requiring explicit knowledge of the spreading codes of the different users.

It is another object of the present invention to provide a novel structure and method for reducing the multiuser interference without requiring explicit knowledge of the relative received power levels of the different users, i.e. a structure and method which is insensitive to the "near-far" problem.

The above objects have been accomplished by making use of a novel scheme for reducing the multiuser interference as claimed in claims 1 and 12.

The multivariate noise-predictive decision-feedback equalizer (MNP-DFE) in accordance with the present invention has the following advantages:

1. The derivation of the multivariate predictor coefficients is decoupled from the derivation of the forward multiuser equalizer coefficients.
2. The multivariate predictor can operate on the output of any bank of linear filters, adaptive or fixed, such as fixed despreaders.
3. An MNP-DFE can easily be combined with soft decision convolutional coding.
4. The forward linear multiuser equalizer and the multivariate predictor of an MNP-DFE optimized under the MMSE (minimum mean squared error criterion) lend themselves to simple adaptive implementations by using the LMS algorithm. The forward linear multiuser equalizer and the multivariate predictor are then updated separately.
5. The forward linear multiuser equalizer of an MNP-DFE configuration can be implemented as a bank of despreaders followed by a matrix of

1   K x K, T-spaced equalizers, or as a bank of K fractional-chip spaced equalizers, where K is the number of simultaneous users.

DESCRIPTION OF THE DRAWINGS
AND NOTATIONS USED

5

The invention is described in detail below with reference to the following drawings:

10   **FIG. 1**   shows a schematic block diagram of a CDMA receiver known in the art.

      FIG. 2A   shows a schematic block diagram of another CDMA system described by Duel-Hallen.

15

      FIG. 2B   shows a schematic block diagram of another CDMA system described by M. Abdulrahman et al.

      FIG. 3   shows a cellular communications system.

20

      FIG. 4   shows a DS/CDMA (direct-sequence Code Division Multiple Access) communications system.

      FIG. 5   shows an equivalent discrete-time multiple-input/

25   multiple-output model.

      FIG. 6   shows a MMSE multiuser linear equalizer.

      FIG. 7   shows an equalizer/detector structure for user 1.

30

      FIG. 8   shows a schematic block diagram of a multivariate noise-predictive decision-feedback equalizer, in accordance with the present invention.

1	FIG. 9	shows a schematic block diagram of another multivariate noise-predictive decision-feedback equalizer, in accordance with the present invention.
5	FIG. 10A, B	show a schematic block diagram of an MNP-DFE, in accordance with the present invention, designed for three users.
	FIG. 11	shows a schematic block diagram of a CDMA Infra Red network in accordance with the present invention.

10

15	$b_k(n)$	data symbol of kth user at time n
	$\{b_k(n)\}$	discrete-time data-symbol sequence of kth user
20	$\underline{b}(n)$	K x 1 data-symbol vector, i.e. $\underline{\hat{b}}(n) = (\hat{b}_1(n), \ldots, \hat{b}_K(n))$
	$\{\underline{b}(n)\}$	discrete-time data-symbol vector sequence
	$s_k(t)$	signature waveform of kth user
25	$\underline{c}_k = \{c_k^i\}_{i=0}^{N-1}$	spreading code of kth user corresponding to signature waveform $S_k(t)$
	w_k	attenuation level of kth user
30	$y_k(n)$	matched-filter output of kth user at time n
	$\{y_k(n)\}$	discrete-time matched-filter output sequence of kth user

1      $\underline{y}(n)$ $K \times 1$ matched-filter output vector, i.e.

$\underline{y}(n) = (y_1(n), \ldots, y_K(n))$

     $\{\underline{y}(n)\}$ discrete-time matched-filter output vector sequence

5

     $r_{kl}(i)$ kl^{th} element of matrix $R(i)$, $i = -1, 0, 1$

     $R_{\underline{\eta}}(i)$ autocorrelation matrix of vector $\underline{\eta}(n)$

10     $S_{\underline{\eta}}(D)$ spectrum of discrete-time vector $\underline{\eta}(n)$

     $S(D)$ transfer function matrix of the equivalent multiple-input/multiple-output channel output

15     $C(D)$ transfer function matrix of the multiple-input/multiple-output equalizer

     $P(D)$ transfer function matrix of the multiple-input/multiple-output (multivariate) predictor

20

     $S_{\underline{e}}(D)$ spectrum of discrete-time prediction error vector $\underline{e}(n)$

25

30

GENERAL DESCRIPTION

Communications System Model:

A cellular system composed of cells 21 and 22, base stations (BS) 15 - 17, and mobile stations (MS) 18 - 20, is shown in Figure 3. As illustrated, two of the BSs are connected to a common radio network controller 23, whereas a third BS 17 is operated by a non co-operating operator (not shown). For a CDMA system, isolation among cells is achieved largely by spreading codes and distance, and somewhat by frequency and time. However, isolation among cells is not ideal, and causes intra- and inter-cell interference. Furthermore, the existence of cooperating or non-cooperating multiple operators in the same geographical area worsens the problem of multiuser interference.

Inter-cell interference can arise from:

- multiuser interference from non-cooperating operators, such as interference from BS 17 to BS 16 and to MS 20 (if BS 17 belongs to a non-cooperating operator);
- multiuser interference from cooperating cellular systems;
- multiuser interference from different cells of the same cellular system, such as between MS 19 and BS 16. Even though MS 19 and BS 16 may desire to communicate, such as during some form of handover to a new cell, the signal from MS 19 may cause interference at BS 16 when BS 16 detects the signal from MS 20.

Intra-cell interference can arise from:

- multiuser interference within a cell of some cellular system, such as at BS 15. For example, BS 15 must detect the signal from MS 18, which is corrupted by the signal from MS 19. BS 15 must also detect the signal from MS 19, which is corrupted by the signal from MS 18.

1   Figure 4 shows a general block diagram of a direct-sequence CDMA (DS/CDMA) communications system model. In this model, a common additive white Gaussian noise (AWGN) channel is shared by synchronous or asynchronous users (1,2, . . . ,K) whose transmitted power is attenuated by

5   different values. Without loss of generality, the attenuation levels $w_1, w_2, \ldots, w_K$ have been lumped together with the corresponding data symbols $b_1(n), \ldots, b_K(n)$. Furthermore, the existence of despreading circuitry 40, 44, 45 at the receiver side has been assumed. This despreading circuitry comprises a despreader 40 and integrate and dump units 44, 45. The

10 transmitter of each user consists basically of a spreading and modulation unit 41. For transmitters located in mobile stations (MS) the delay units 42 represent the relative delay $(\tau_1, \ldots, \tau_K)$ in transmission among the different MS users. The summation unit 43 then indicates the process of superposition of signals when transmitted through the physical medium. On

15 the other hand, if the transmitters are located in the base station (BS), then there is no relative delay between the different users and the corresponding units 42 can be eliminated. In this case, the summation unit 43 is a part of the BS transmitter.

20 The data sequence $\{b_k(n)\}$ of the kth user is represented by the D-transform

$$b_k(D) = \sum_n b_k(n) \, D^n \, , \tag{1}$$

25

where $k = 1,2, \ldots, K$ and n is an integer. In vector notation

$$\underline{b}(n) = (b_1(n), b_2(n), \ldots, b_K(n)) \tag{2}$$

30 represents the data sequence vector and $\underline{b}(D)$ the corresponding D-transform. The symbols are transmitted at rate $1/T$, are uncorrelated, and have an average energy of unity. To each user corresponds a signature waveform

$$s_k(t) = \sum_{i=0}^{N-1} c_k^i \, p_c(t - iT_c) \qquad 1 \leq k \leq K , \qquad (3)$$

where $p_c(t)$ is the chip pulse shape, $N = T/T_c$ is the spreading factor, and $\underline{c}_k = \{c_k \in (-1,1)\}_{i=0}^{N-1}$ is the spreading code of the kth user.

Usually, the spreading function at the transmitter of a BS or MS terminal is performed by multiplying the transmitted data sequence $\{b_k(n)\}$ with the signature waveform $s_k(t)$. An alternative implementation of the spreader 41 (and despreader 40) is by making the spreading code the impulse response of a filter. Therefore, the transmitted spread signal is the result of a convolution operation as opposed to a multiplication operation. The advantage of the latter approach is that it allows for spreading codes which are longer (or shorter) than one symbol period, while maintaining time-invariant properties of the multiuser equalizers involved at the receiver. For the sake of notational simplicity, spreading via multiplication, as illustrated in Figure 4, has been assumed in the following.

The receiver observes the superposition $\underline{r}(n)$ of the K user signals in the presence of additional white Gaussian noise $\eta(t)$ (AWGN) with variance σ^2, i.e.

$$r(t) = \sum_{n=-\infty}^{\infty} \sum_{k=1}^{K} w_k b_k(n) \, s_k(t - nT - \tau_k) + \eta(t) \qquad (4)$$

where w_k^2 denotes the received power of the kth user and $0 \leq \tau_1 \leq \tau_2 \ldots \tau_K \leq T$ represent the relative time delays.

1   After matched filtering (by means of 40, 44, and 45) and symbol-rate
     sampling at the samplers 45, the set of sufficient statistics $\{\underline{y}(n)\}$ are
     obtained, where

5
$$\underline{y}(n) = (y_1(n), y_2(n), \ldots, y_K(n)) \ , \tag{5}$$

     and

10
$$y_k(n) = \int r(t) \ s_k(t - nT - \tau_k)dt \qquad 1 \leq k \leq K \tag{6}$$

     denotes the output of the kth matched-filter. In vector notation the
     matched-filter outputs can be written as

15
$$\underline{y}(n) = R(1) W\underline{b}(n - 1) + R(0) W\underline{b}(n) + R(-1) W\underline{b}(n + 1) + \underline{\eta}(n) \ . \tag{7}$$

     (See also the above mentioned article "Minimum probability of error for
     asynchronous Gaussian multiple access channels", by S. Verdú). The
20   essential system parameters are therefore represented by the $K \times K$
     cross-correlation matrices $R(i)$, $i = -1, 0, 1$, and the diagonal matrix
     $W = diag(w_1, w_2, \ldots, w_K)$. The kl^{th} element of $R(i)$ is computed by

25
$$r_{kl}(i) = \int s_k(t - \tau_k) \ s_l(t + iT - \tau_l)dt \qquad 1 \leq k,l \leq K \ . \tag{8}$$

     Note that $R(0)$ is symmetric and $R(1)$ is upper triangular with zero diagonal
     elements. Furthermore, $R(-1) = R(1)^T$, where T denotes the complex
     conjugate transpose.

30
     It can also be shown that the autocorrelation matrix of the noise vector at
     the output of the matched-filters 40, 44 is given by

15

$$R_{\underline{\eta}}(i) = E \{ \underline{\eta}(n+i)\underline{\eta}(n)^T \} = \sigma^2 R(i) , \qquad i = -1, 0, 1 . \qquad (9)$$

Equations (7) and (9) give rise to an equivalent discrete-time multiple-input/multiple-output model for a CDMA system. Figure 5 shows a block diagram of this model. Using equation (7), it can be shown that the transfer function matrix of the equivalent channel 50 is given by

$$S(D) = R(1) D + R(0) + R(-1) D^{-1} . \qquad (10)$$

Similarly, the spectrum of the discrete-time noise vector $\underline{\eta}(n)$ is given by

$$S_{\underline{\eta}}(D) = \sum_i R_{\underline{\eta}}(i) D^i = \sigma^2 S(D) . \qquad (11)$$

Equations (7) and (9), or equivalently (10) and (11), translate the joint detection problem of K asynchronous or synchronous CDMA users to a problem of estimating a vector sequence emerging from a multiple-input/multiple-output discrete-time channel in the presence of additive colored vector noise. It is also clear from the same equations the deterministic nature of the multiuser interference and its dependence on the auto- and cross-correlation properties of the short spreading codes. Thus, some of the equalization techniques developed for multiplexed signals over multiple-input/multiple-output channels with intersymbol interference (ISI) and crosstalk (see the already mentioned article "Equalizers for multiple input/multiple output channels and PAM systems with cyclostationary input sequences", A. Duel-Hallen, IEEE J. Select. Areas Commun., Vol. 10, No. 3, pp. 630-639, Apr. 1992, and the references therein) can in principle be applied, to solve similar problems in CDMA systems.

1   MMSE Linear Multiuser Equalizer:

If further processing of the matched-filter outputs $\{\underline{y}(n)\}$ is restricted to be linear, then we arrive at a linear receiver structure which takes the form of a
5   network of K x K, T-spaced, infinite-length transversal equalizers followed by a bank of K memoryless detectors. Let C(D) denote the K x K equalizer transfer matrix. The mean squared error criterion is

$$E \{ | \underline{x}(n) - W \underline{b}(n) |^2 \} , \tag{12}$$

10

where $\underline{x}(n)$ denotes the output of the multiuser equalizer 60, as illustrated in Figure 6. Applying the orthogonality principle, one obtains the transfer matrix C(D) of this multiuser equalizer 60 which gives the MMSE. That is,
15   C(D) is selected such that

$$E \{(\underline{x}(n + i) - W \underline{b}(n + i)) \underline{y}(n)^T\} = 0 \qquad \forall \ i \ . \tag{13}$$

20   Equation (13) leads to $R_{\underline{x}, \underline{y}}(i) = R_{W\underline{b}, \underline{y}}(i)$, or equivalently using the cross-spectrums in the D-domain $S_{\underline{x}, \underline{y}}(D) = S_{W\underline{b}, \underline{y}}(D)$. Hence,

$$C(D) (S(D) W^2 + \sigma^2 I) S(D) = W^2 S(D) , \tag{14}$$

25   where I represents the K x K identity matrix. Therefore, the transfer matrix C(D) of the multiuser equalizer 60, based on the MMSE criterion, is

$$C(D) = W^2 (S(D) W^2 + \sigma^2 I)^{-1} . \tag{15}$$

30

An equalizer/detector structure, in accordance with the present invention, for the first user is shown in Figure 7. In this case the transfer function $c_{11}(D), \dots , c_{1k}(D)$ are the elements of the first row of the transfer matrix C(D). Three units 61 of this first row are schematically shown in Figure 7. Let

1    $\underline{\eta}'(D) = \underline{x}(D) - W\underline{b}(D)$ denote the D-transform of the noise and residual interference vector at the output of the multiuser equalizer 60. Then,

$$\underline{\eta}'(D) = (C(D) S(D) - I) W \underline{b}(D) + C(D)\underline{\eta}(D) \,, \tag{16}$$

5

and its spectrum is given by

$$S_{\underline{\eta}'}(D) = (C(D) S(D) - I) W^2 (C(D^{-1}) S(D^{-1}) - I)^\mathsf{T} + \sigma^2 C(D) S(D) C(D^{-1})^\mathsf{T} \,, \tag{17}$$

10

where the first term represents the spectrum of the residual interference and the second term represents the spectrum of the output noise. Using the matrix inversion lemma, it can be shown that

15

$$S_{\underline{\eta}'}(D) = \sigma^2 C(D) \,. \tag{18}$$

Thus, the MMSE of the kth user can be computed by simply integrating the kk^{th} diagonal element of the matrix $S_{\underline{\eta}'}(D)$ on the unit circle, i.e.

20

$$E\{ |\eta'_k(n)|^2 \} = \frac{1}{2\pi} \int_{-\pi}^{\pi} (\sigma^2 W^2 (S(e^{j\omega}) W^2 + \sigma^2 I)^{-1})_{kk} \, d\omega \,. \tag{19}$$

25

In contrast to a ZF multiuser equalizer, the relative power levels of the different users appear explicitly in the MMSE equalizer's transfer matrix C(D). Their effect on the MMSE has been studied via numerical computation. It has been found that an infinitely long MMSE multiuser equalizer is almost insensitive to the different power levels. This result demonstrates the inherent "near-far" resistance of the present MMSE multiuser linear equalizer 60.

18

1   MMSE Multivariate Noise-Predictive Decision Feedback Equalizer:

The MSE of the noise and residual interference vector $\underline{\eta}'(D)$ at the output of a linear multiuser equalizer can be further reduced by multivariate

5   prediction. The idea is to use a multivariate predictor which operates as a whitening multiple-input/multiple-output filter on the vector $\underline{\eta}'(D)$. This argument motivates the multivariate noise-predictive decision-feedback equalizer structure shown in Figure 8. It consists of a forward ZF or MMSE linear multiuser equalizer 80, as has been defined in the previous section,

10   followed by a multivariate predictor 81. This section describes the basic principles of this approach. Let P(D) denote the general multivariate predictor K x K transfer matrix, i.e.

15
$$P(D) \;=\; P(0) + P(1)D + P(2)D^2 + \; \ldots \; = \; \sum_{i=0}^{\infty} P(i)D^i \quad , \qquad (20)$$

where P(0) is a lower diagonal matrix with zero diagonal elements. Let also $\tilde{\underline{\eta}}(n)$ represent the multivariate predictor output vector.   Then

20      $\tilde{\underline{\eta}}(n) = P(D)\,\underline{\eta}'(n)$. Note that the ith component of the predictor output vector $\tilde{\underline{\eta}}(n)$ depends not only on the past vectors $\underline{\eta}'(n-1), \underline{\eta}'(n-2), \; \ldots \;$, but also on the present values $\eta'_{i+1}(n), \; \ldots \;, \eta'_K(n)$. Thus, the multivariate prediction process in accordance with the present invention, can be viewed as exploiting both past information and user-order. The error vector $\underline{e}(D)$ at

25   the input of the memoryless detector 82 can be expressed as

$$\underline{e}(D) \;=\; \underline{z}(D) - W\underline{b}(D) \;=\; \underline{x}(D) - \tilde{\underline{\eta}}(D) - W\underline{b}(D) \;=\; \underline{\eta}'(D) - \tilde{\underline{\eta}}(D) \quad (21)$$

30   thus,

$$\underline{e}(D) \;=\; \underline{\eta}'(D) - P(D)\,\underline{\eta}'(D) \qquad\qquad (22)$$

19

is the multivariate prediction error. The inverse spectral matrix of the wide sense stationary stochastic process $\{\underline{\eta}'(n)\}$ admits the following factorization:

$$S_{\underline{\eta}'}(D)^{-1} = H(D^{-1})^T H(D) \tag{23}$$

where, $H(D) = H(0) + H(1)D + H(2)D^2 \ldots$, and $H(0)$ is a lower triangular nonsingular matrix. Equivalently,

$$S_{\underline{\eta}'}(D)^{-1} = H'(D^{-1})^T (H^d(0))^2 H'(D) \tag{24}$$

where $H^d(0)$ is a diagonal matrix whose elements are the diagonal elements of $H(0)$ and $H'(D) = H^d(0)^{-1} H(D)$. Using equation (22), one obtains

$$S_{\underline{e}}(D) = (I - P(D)) S_{\underline{\eta}'}(D) (I - P(D^{-1}))^T . \tag{25}$$

Therefore, the transfer matrix of the predictor 81 is given by

$$P(D) = I - H^d(0)^{-1} H(D) , \tag{26}$$

and the prediction error spectral matrix

$$S_{\underline{e}}(D) = H^d(0)^{-2} . \tag{27}$$

Thus, the MMSE at the input of the kth memoryless detector, i.e. the MMSE of the kth user, is the kk^{th} diagonal element of the diagonal matrix in equation (27). The equivalence in performance of the conventional multiuser DFE and the noise-predictive multiuser DFE can be established as follows. Define

1

$$F(D) \;=\; (I - P(D))\,C(D) \;=\; \frac{1}{\sigma^2}\, H^d(0)^{-1} H(D^{-1})^{-T} \;, \qquad (28)$$

and

5

$$B(D) \;=\; P(D) \;=\; I - H^d(0)^{-1}\,H(D) \;. \qquad (29)$$

One can easily see now that, $F(D)$ and $B(D)$ are the transfer matrices which
10 define forward and feedback sections of an MDFE (see the above cited IEEE
J. Select. Areas article of A. Duel-Hallen). Thus an infinite long MNP-DFE
and an infinite long MDFE have the same performance. From an
implementation point of view though, those two schemes are different.

15 Figure 9 shows the basic principle of a multivariate predictor structure. The
multiuser interference part of the signal vector $\underline{x}(D)$ is being isolated by
using the decision vector $\hat{\underline{b}}(D)$. The isolation of said multiuser interference
part is carried out by means for extracting interference signals 83. The
multivariate predictor 81 operating both in time and user order produces an
20 output vector $\tilde{\underline{\eta}}(D)$ which is as close as possible in MMSE sense to the
multiuser interference vector $\underline{\eta}'(D)$. Subtracting the multivariate predictor
output $\underline{\eta}'(D)$ from the input vector $\underline{x}(D)$ results in a minimization of the
multiuser interference at the input of the quantizer 82.

25 CDMA System Design Considerations:

In the following section some general aspects of the present CDMA system
are discussed. In practical applications the MMSE multiuser linear
equalizer and multivariate predictor have finite lengths. For finite lengths
30 and known cross-correlation matrices, the coefficients of the multiuser
equalizer can be obtained by simply solving a set of linear equations. In the
case of a multiuser noise-predictive decision feedback equalizer the solution
begins by obtaining first the coefficients of the forward linear multiuser

1 equalizer. The coefficients of the multivariate predictor are then the solution of a set of generalized normal equations. Adaptive equalizers have the property of converging dynamically to the correct set of coefficients without explicitly solving a system of equations.

5

Note that the implementation of the equalizers - and embodiments of the present invention - do not depend on whether transmission to and from the base station is asynchronous or synchronous. Synchronous transmission will improve the orthogonality properties of the spreading codes and will

10 marginally improve the performance of a multiuser equalizer.

The linear MMSE multiuser equalizer, in accordance with the present invention, can be implemented as a network of, K x K, T-spaced equalizers, or as a bank of K fractional-chip spaced equalizers. In the latter case, there

15 is no need to explicitly implement the despreading function separately. The fractional-chip spaced equalizer has the property of synthesizing both the despreading and the equalizing functions. The practical advantage of MMSE equalizers is that they lend themselves to simple adaptive implementation. Thus, for a fading channel and unknown cross-correlation

20 functions, standard adaptation algorithms can be applied. The adaptation algorithms can operate in reference-directed or decision-directed mode. In environments where the channel changes very slowly relative to the symbol rate, it will be easier for the equalizer to track the variations. In rapidly changing environments, additional techniques such as channel sounding

25 may be necessary. However, note that a multiuser equalizer does not invert the channel frequency response but rather the spectrum of the correlation matrices which are formed from the different spreading codes. Hence, in this regard the tracking problem of a multiuser equalizer should be in general easier than the tracking problem of a conventional single-input

30 single-output equalizer over a fast-fading frequency selective channel.

One of the major practical advantages of the present multiuser noise-predictive decision feedback equalizer is that the adaptation of the

forward linear multiuser equalizer is decoupled from that of the multivariate predictor. As a consequence, the multivariate predictor can always be disconnected or connected without affecting the normal operation of the system. For example, it may be desirable to disconnect completely the multivariate prediction operation if high error propagation due to feedback in a fast fading situation is observed. On the other hand, in a heavy shadowing situation applying partial multivariate noise prediction on users with relatively large power could substantially improve the performance of weak users who would otherwise suffer high error rates.

The base station (BS) usually has knowledge of the spreading code of all users (MS) in a particular cell and can afford receivers with higher complexity for implementing joint multiuser equalization/detection schemes. Therefore, the present multiuser noise-predictive decision feedback equalization is a promising approach for joint equalization/detection at the base station. The knowledge of the spreading codes can be used to aid fast convergence and/or retraining of the equalizers if necessary. This can be achieved by simply presetting the forward multiuser equalizer coefficients with the corresponding known spreading codes, or possibly by calculating the values of the multiuser linear equalizer coefficients using knowledge of the spreading codes, delays, powers and multipath profiles.

Multipath reception at the base station (BS) can be achieved by a RAKE receiver in combination with the despreaders followed by a multiuser noise-predictive decision feedback equalizer. In the case of fractional-chip spaced implementation of the joint equalization/detection receiver, multipath reception is inherently and automatically performed by the forward fractional-chip spaced multiuser equalizer. The multiuser equalizer then automatically gives the optimum combining of multipath components in the sense that it adapts to the MMSE solution. For convolutionally encoded data the problem of reliable delayed decisions from the path memory of the Viterbi decoders for decision feedback can efficiently be solved by choosing judiciously the parameters of the interleaver/deinterleaver pairs.

1

Figures 10A and B show an exemplary embodiment of the structure of a multivariate noise-predictive decision-feedback equalizer (MNP-DFE) for joint equalization/detection of K = 3 simultaneous users. The forward

5   section 90 consists of a bank of K = 3 fractional-chip spaced equalizers. The nine delay elements 92, of said forward section 90, provide for a delay of T_c/q. The coefficients of the multiuser equalizer are spaced at T_c/q intervals, where q is a ratio of integers. The multivariate feedback predictor, see Figure 10B, consists of a bank 91 of $K^2 = 9$ FIR (finite impulse response)

10   T-spaced filters. Each of said T-spaced filters comprises two delay elements 93 providing for a delay T. The same Figures also show the error signals $e_{1i}(n)$ and $e_{2i}(n)$, $i = 1,2,3$ which can be used for updating the forward multiuser linear equalizer coefficients and the multivariate feedback predictor coefficients, respectively.

15

An important feature of the MNP-DFE is that it allows interference prediction and subtraction not only in time but also in user order. Note that in a synchronous CDMA system, interference prediction takes place only in user order. In this case, the feedback multivariate predictor consists of

20   $K(K-1)/2$ single-tap filters. This is also the case in an asynchronous CDMA system (see Figures 10A, 10B) if one assumes that only the rightmost column of coefficients in the bank of feedback filters 91 are present.

25   Except for the time 0 coefficients, all coefficients of the present MNP-DFE are adapted in a conventional manner, i.e. by use of techniques like the LMS algorithm. An example of how the time 0 coefficients are different is shown in Figures 10A, 10B for the detection over the user order 1,2, then 3. In this case, the only time 0 coefficients that are adapted are the prediction

30   coefficients p_{21}, p_{31}, and p_{32}. The coefficients labelled 0 are always zero, whereas the The coefficients labelled 0m are presently zero, and only for this particular detection order. However, the last non zero values are stored elsewhere so that they can be restored if there is an appropriate

1   change in the order of the user's is detected. The determination of the user
order can be based on estimations of various criteria among the users, such
as received signal powers, or mean-square errors (MSEs) at the output of
the bank of linear filters 91. In any case, the determined user order will
5   likely change due to channel impairments such as fading or noise. Changes
in user order are implemented by saving the current prediction coefficients
and loading in a new set, corresponding to the new user order.

The present invention is also applicable in CDMA Infra Red (IR) networks. A
10   CDMA based IR system is shown in Figure 11. The mobile stations 110 are
equipped with spreading circuitry 111 and opto-electronic transmission units
112. At the base station after photodetection, by means of an opto-electronic
receiver 113, and spreading, carried out by despreaders 40, the signals of
the different users are processed by an MNP-DFE 115 in order to reduce
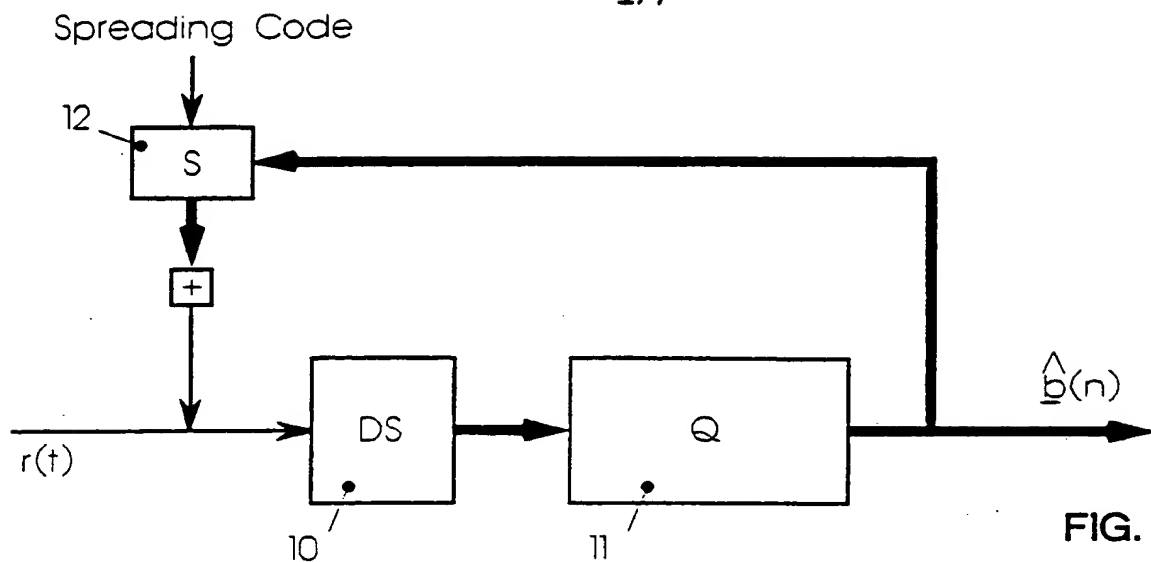15   multiuser interference.

20

25

30

CLAIMS

1. Apparatus for reducing the multiuser-interference of input signals $\underline{x}(D)$, said apparatus being part of or attached to a receiver, comprising: a multivariate predictor (81) and a decision quantizer (82), said multivariate predictor (81) operating on interference signals $\underline{\eta}'(D)$ provided by means for extracting interference signals (83), said interference signals $\underline{\eta}'(D)$ being obtained from said input signals $\underline{x}(D)$ and from output signals $\underline{\hat{b}}(D)$ available at an output of said decision quantizer (82), said multivariate predictor (81) feeding its output signals $\underline{\tilde{\eta}}(D)$ into said input signals $\underline{x}(D)$.

2. The apparatus of claim 1, further comprising a matrix of forward filters (80) for a first interference reduction at its input.

3. The apparatus of claim 1, further comprising a bank (90) of fractional-chip spaced filters for a first interference reduction is situated at its input.

4. The apparatus of claim 1, wherein said means for generating interference signals (83) subtract said output signals $\underline{\hat{b}}(D)$ from said input signals $\underline{x}(D)$.

5. The apparatus of claim 1, wherein said predictor comprises a network (91) of K x K T-spaced filters.

6. The apparatus of claim 5, wherein said predictor comprises means for subtracting the multivariate predictor output signals $\underline{\tilde{\eta}}(D)$, provided at the outputs of said network (91) of K x K T-spaced filters, from said input signals $\underline{x}(D)$.

7. The apparatus of claim 2, wherein each forward filter (80) of said matrix is either

1   •   a zero-forcing (ZF) linear equalizer, or

     •   a minimum-mean-square error (MMSE) linear equalizer.

8. The apparatus of claim 1, wherein said quantizer (82) is a Viterbi
5   decoder for decoding convolutionally encoded data.

9. The apparatus of any of the preceding claims, comprising means for
determining prediction errors $\underline{e}(D)$ being used for updating the
prediction coefficients of said predictor.

10

10. CDMA communications system wherein a base station (BS) and/or a
mobile station (MS) comprise(s) an apparatus in accordance with any of
the preceding claims.

15 11. A CDMA communications system in accordance with claim 10, which is
also equipped to transmit and receive TDMA- or FDMA-based traffic.

12. Method for reducing the multiuser-interference of input signals $\underline{x}(D)$
comprising the steps:
20   •   extracting interference signals $\underline{\eta}'(D)$ from said input signals $\underline{x}(D)$ by
using output signals $\underline{\hat{b}}(D)$ of a decision quantizer (82),
     •   generating multivariate predictor output signals $\underline{\tilde{\eta}}(D)$ by taking said
separated interference signals $\underline{\eta}'(D)$ as inputs, and
     •   reducing the noise and residual interference signals of said input
25   signals $\underline{x}(D)$ by subtracting said multivariate predictor output
         signals $\underline{\tilde{\eta}}(D)$ from said input signals $\underline{x}(D)$.

13. The method of claim 12, wherein a first interference reduction step is
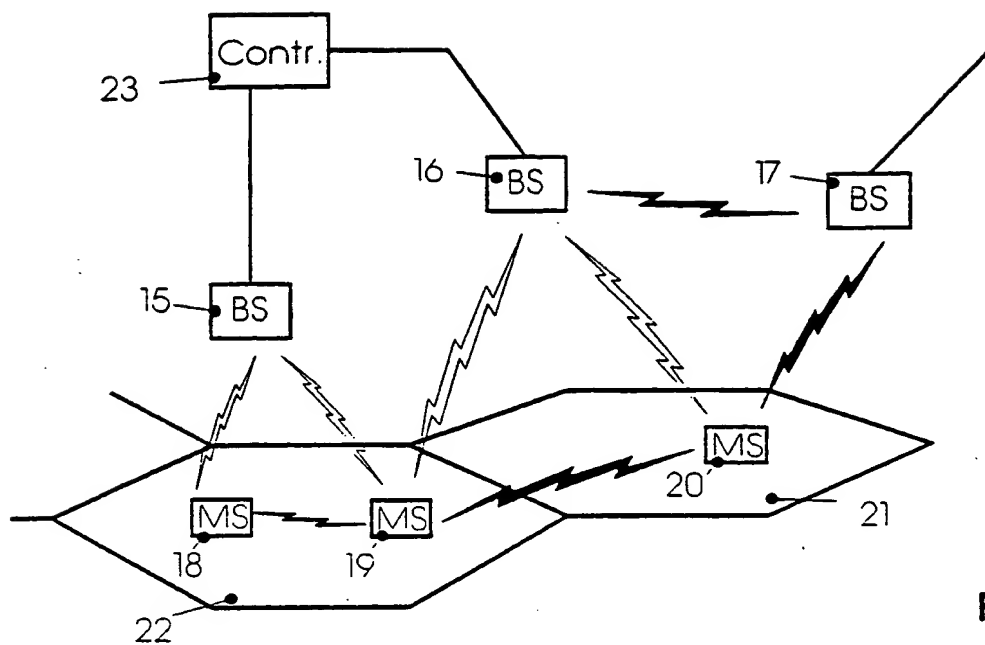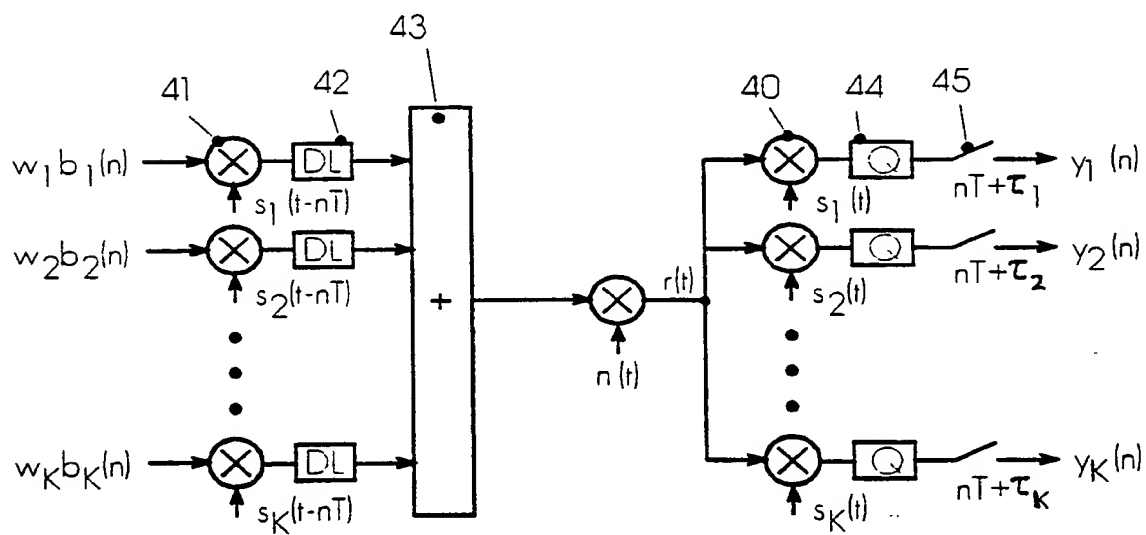carried out prior to said extraction of interference signals $\underline{\eta}'(D)$.
30

Spreading Code

12

S

+

r(t)

DS

Q

$\hat{\underline{b}}(n)$

10

11

FIG. 1

17

$\underline{y}(n)$

K x K matrix filter

$\underline{z}(n)$

13

Q

$\hat{\underline{b}}(n)$

K x K matrix filter (FBF)

14

FIG. 2A

Tc/2

r(t)

Fraction. spaced filter

nT

$z_k(n)$
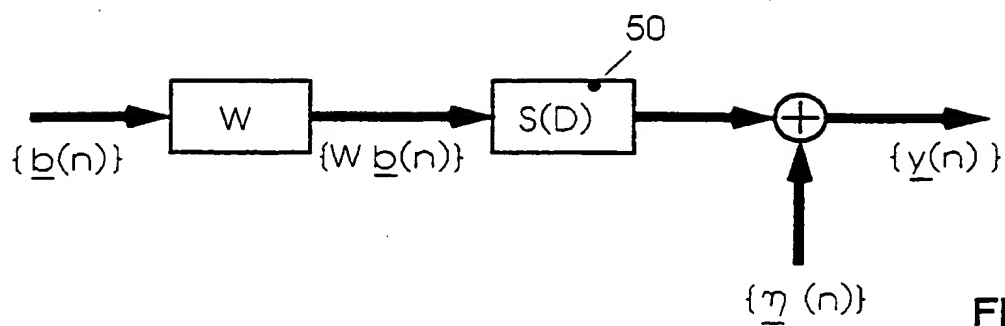
15

Q

$\hat{b}_k(n)$

filter (FBF)

16

FIG. 2B
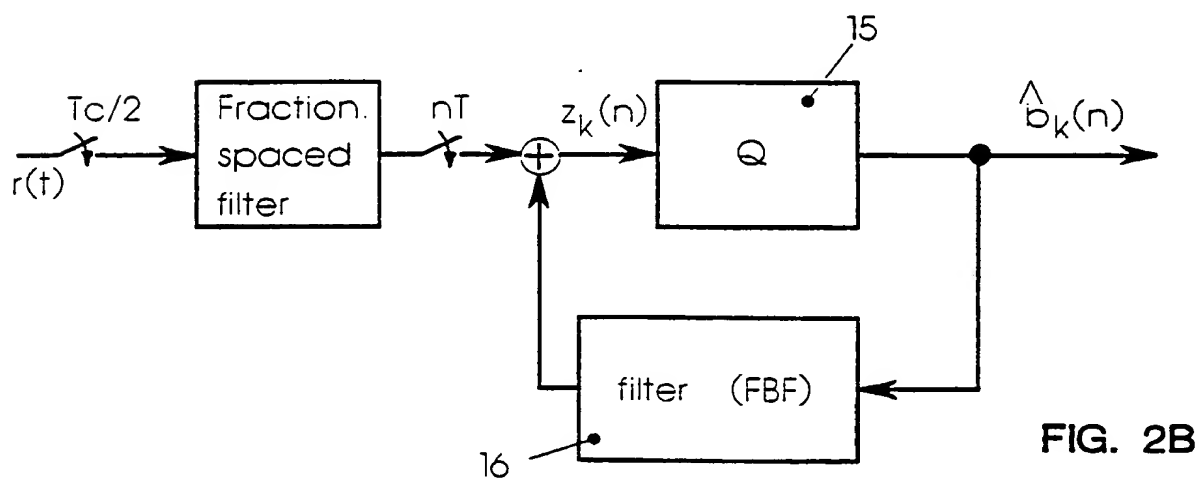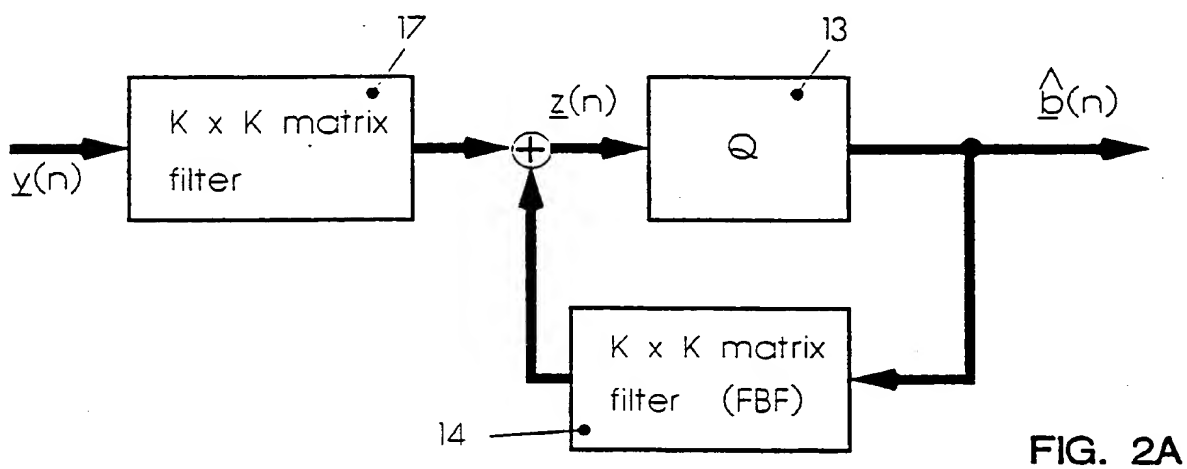
FIG. 3

FIG. 4

FIG. 5
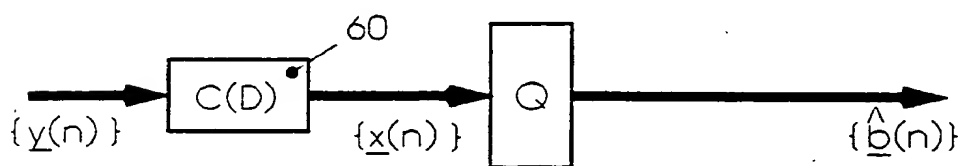
FIG. 6

FIG. 7

4/7

FIG. 8

FIG. 9
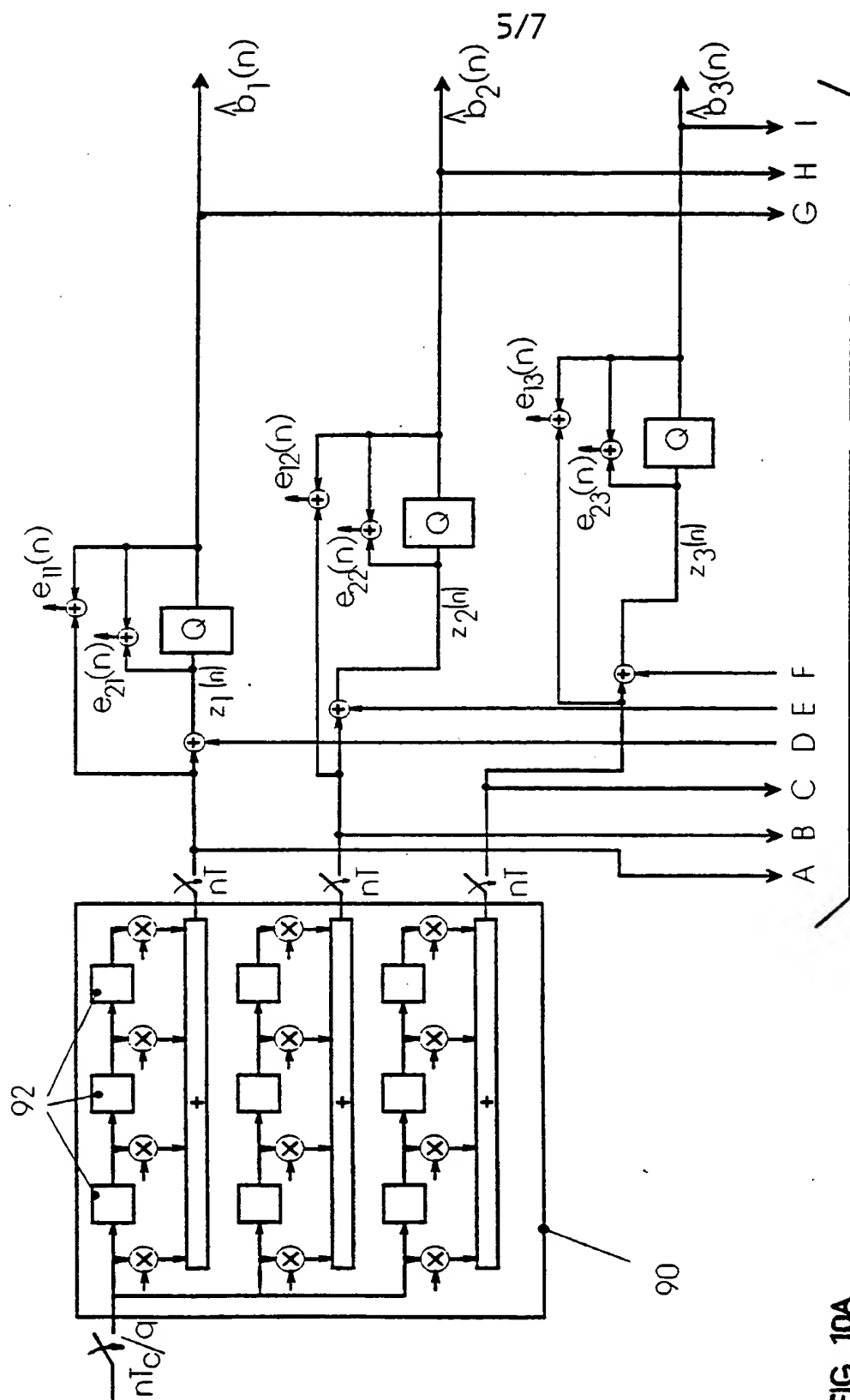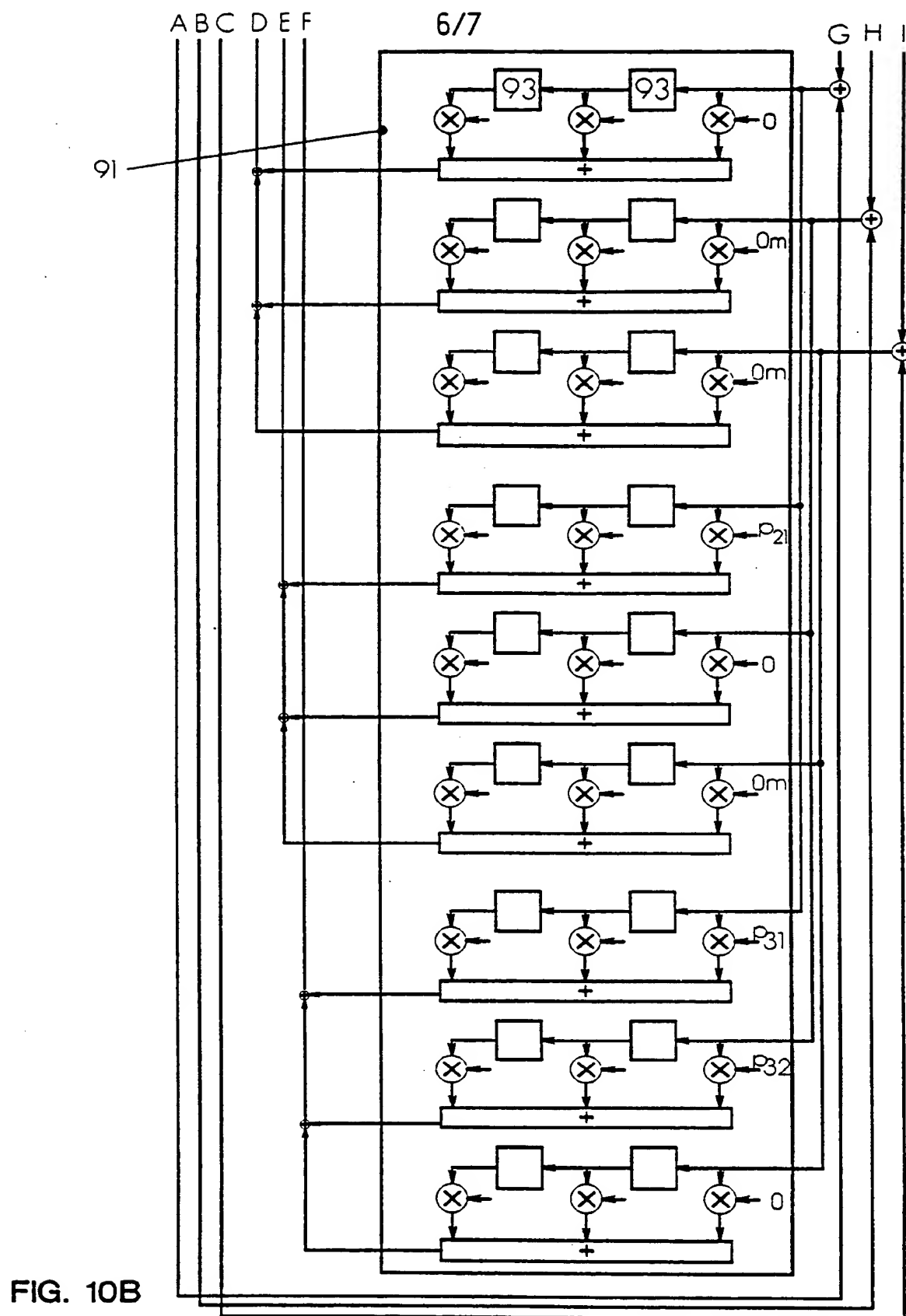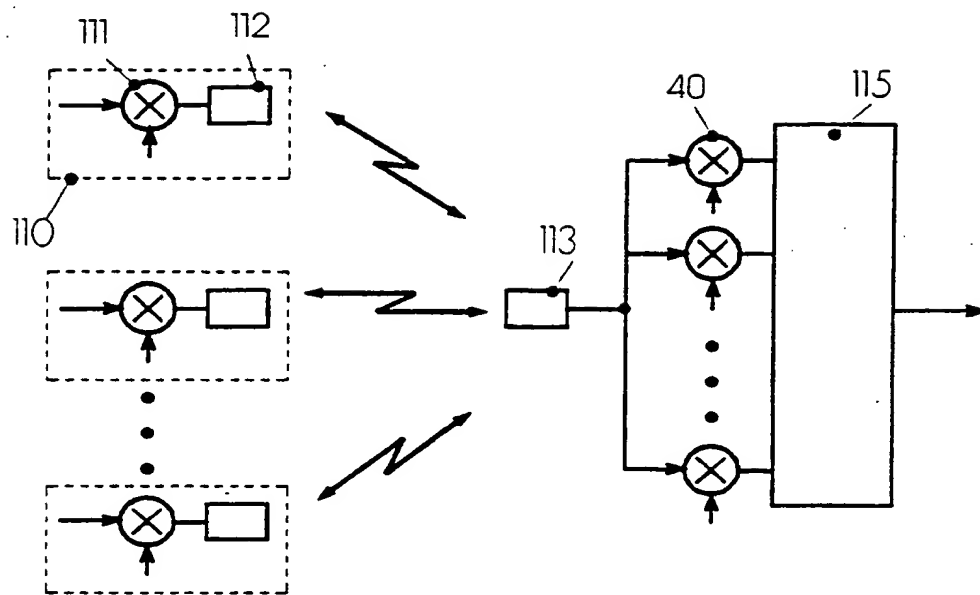
FIG. 10A

FIG. 10B

●   ●

FIG. 11

INTERNATIONAL SEARCH REPORT

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6   H04B7/26   H04L25/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6   H04J   H04B   H04L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	ELECTRONICS LETTERS, vol.30, no.3, 3 February 1994, STEVENAGE,UK; pages 192 - 193, XP431313 P.N.MONOGIOUDIS ET AL. 'Performance of adaptive nonlinear NEFAR CDMA receiver architecture' see the whole document --- -/--	1-13

[X] Further documents are listed in the continuation of box C.

[X] Patent family members are listed in annex.

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"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
30 September 1994	25. 10. 94

Name and mailing address of the ISA	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax (+31-70) 340-3016	Bischof, J-L

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page 1 of 2

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	IEEE JOURNAL ON SELECTED AREAS IN COMMUNICATIONS, vol.11, no.7, 1993, NEW-YORK,US; pages 1058 - 1066, XP400015 A.KLEIN ET AL 'Linear Unbiased Data Estimation in Mobile Radio Systems Applying CDMA' see page 1058, right column, line 4 - line 30; figures 1,3 see page 1059, left column, line 23 - line 27 ---	1,7-12 •
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A	US,A,5 031 195 (CHEVILLAT ET AL) 9 July 1991 see column 2, line 15 - line 57; figures 1,2 ---	1,5,6,8, 12
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A	EP,A,0 534 489 (NEC CORPORATION) 31 March 1993 see claim 1; figure 1 -----	1,3,12

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US-A-5031195	09-07-91	NONE		
US-A-3875515	01-04-75	NONE		
EP-A-0534489	31-03-93	JP-A-	5090904	09-04-93